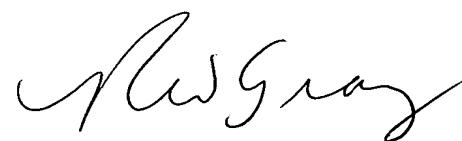


UNITED STATES PATENT AND TRADEMARK OFFICE

I, Roger Walter GRAY MA, DPhil, CPhys,
translator to RWS Group plc, of Europa House, Marsham Way, Gerrards Cross,
Buckinghamshire, England declare;

1. That I am a citizen of the United Kingdom of Great Britain and Northern Ireland.
2. That I am well acquainted with the French and English languages.
3. That the attached is, to the best of my knowledge and belief, a true translation into the English language of the specification in French filed with the application for a patent in the U.S.A. on
- under the number
4. That I believe that all statements made herein of my own knowledge are true and that all statements made on information and belief are true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the patent application in the United States of America or any patent issuing thereon.



For and on behalf of RWS Group plc
The 20th day of March 2000

**PROCESS FOR MANUFACTURING INFRASTRUCTURES BASED ON
VITRIFIED BLAST-FURNACE SLAG AND ADDITIVE USED**

The present invention relates to the construction of road and motorway infrastructures, such as base courses and foundation courses of roads, or of civil engineering infrastructures, such as rafts for building foundations, for airport parking or storage areas, for railway platforms or for port quays or wharfs. Generically, this collection of uses will be referred to hereafter by the term "infrastructures".

It is well known in the manufacture of these infrastructures to use mixes of aggregates, of a hydraulic binder, comprising a slag and an activator, and of water (the gravel-slag or sand-slag technique). Next, the mix is spread out over the surface to be treated and is compacted according to particular specifications.

The aggregates consist, in a known manner, of grit or sand, for example, coming from quarries.

The slag used is a by-product of the manufacture of pig iron in blast furnaces and is consequently inexpensive. It is essentially composed of three oxides, namely CaO , SiO_2 and Al_2O_3 , which may be in the form of oxides, silicates, aluminates or aluminosilicates. On leaving the blast furnace, the slag is vitrified and made into particulate form, essentially using two methods. According to the first method, the slag leaving the blast furnace at 1500°C is sent, in the form of a fluid stream, into a tank whose walls include water jets; the slag forms particles having surface asperities: it is called "granulated" slag. The particles of granulated slag have dimensions of less than 5 mm, their average size generally being about 0.5 mm; the granulated slag contains approximately 1% of fines having a particle size of less than 80 micrometers. According to a second method, the slag is cooled by mechanically and hydraulically spraying it at high speed into the air; the particles

are in the form of nodules having a spheroidal shape and a foam structure; it is called "pelletized" slag. The particles of pelletized slag have a particle size of less than 80 mm, 95% of particles generally having 5 average sizes of less than 20 mm; the pelletized slag contains virtually no fines.

The granulated or pelletized slag is generally used in preground form. By pregrinding, the particle size of the entire product is reduced and the 10 proportion of fines of less than 80 μm is increased.

It is also known to add an activator in pulverulent form to the slag. The activation of the vitrified blast-furnace slag consists, firstly, in the presence of water, in attacking the slag with a basic 15 agent, the purpose of which is to dissolve a small amount of slag. Thus, by successive crystallization from the aqueous phase, solid hydrated compounds are formed, which results in the mix setting and hardening. The activator is defined in French Standard 20 NF P 98-107; it may consist of lime, calcium sulphate or both these, it may also contain soda or potash, silica and also a product having, in addition, hydraulic binder properties.

The mix of aggregates, slag, activator and 25 water must principally have the following properties.

Firstly, the mix must not set immediately, so as to be able to be spread out over the ground. It is desirable to have a workability time at least greater than 12 hours, generally between 15 and 30 hours. When 30 the mix is spread out over the ground, it is compacted using a specified process and to a specified value. Setting then starts and may last 4 to 5 years, the mix after compacting nevertheless being already sufficiently load-bearing in order for it to be 35 possible, in particular, to drive over it immediately.

Secondly, the compacted mix must comply with mechanical performance standards. The mechanical performance characteristics taken into account are the 360-day tensile strength (R_t) and the 360-day elastic

modulus (E), the values of which are estimated from test pieces manufactured in the laboratory. It has been found that the 360-day mechanical performance characteristics depended on the particle size of the 5 granulated or pelletized slag and that it was favourable to use a preground slag, the particles of which are smaller than 2 mm and contain approximately 10% of fines.

However, the storage properties of the slag 10 depend on the composition of the latter. This is because, when an iron ore coming from mines in Lorraine (minette ore) is used in blast furnaces and worked according to the Thomas process, a stable and storable preground slag is obtained and it is possible to 15 achieve 360-day mechanical performance characteristics according to the standards, even after the preground slag has been stored. However, when the slag comes from the treatment of another ore, for example, haematite, the preground slag very often does not comply with the 20 mechanical performance standards; this is because it has been found that, during storage, the proportion of fines decreases in a random fashion during storage; it may thus go from 10 to 4% in a few hours.

Now, it seems that the fines content of the 25 slag used is an essential datum for achieving the required performance characteristics of the mix. The object of the invention is therefore to guarantee a sufficient content of fines in the slag at the time of mixing in the mixer and to obtain workable mixes which 30 meet the 360-day performance standards.

The subject of the invention is therefore a process for constructing infrastructures, especially civil engineering infrastructures or road infrastructures, in which aggregates, vitrified blast- 35 furnace slag, a pulverulent activator and water are mixed together, and the mix is spread out over the ground, compacted and left to harden, characterized in that a particulate slag and a ready-prepared additive containing, on the one hand, the activator and, on the

other hand, dry ground vitrified slag having a particle size of less than 500 μm are added to the aggregates. Preferably, the particulate slag added to the aggregates is an as-granulated or as-pelletized slag 5 which is not preground.

The ground vitrified slag is obtained by passing a granulated or pelletized slag through a suitable mill, for example a ball mill; the slag is preferably dried during the grinding until its water 10 content is less than 0.5% by weight. The ground slag has a particle size of less than 500 μm , preferably less than 100 μm , for at least 80% by weight.

The activator may be any known activator. However, it is preferred to use an activator 15 consisting, for more than 95% by weight, of lime or of calcium sulphate or, more particularly preferably, of a mixture of lime and calcium sulphate; the activator may optionally contain small amounts of soda or potash. Advantageously, the activator has an average particle 20 size of between 0 and 500 μm for at least 95% of its weight and a moisture content of less than 0.5% by weight.

For more than 95% by weight, the additive 25 preferably consists of a mixture having the following formulation by weight:

- calcium sulphate	25 to 45 %
- lime	2 to 6 %
- dry ground vitrified slag	qsp 100 %.

Further known formulation adjuvants for this 30 type of mix (aggregates/slag/activator/water) may be introduced into the additive, such as a deflocculant, a setting accelerator or retarder, or steelworks scoria.

The amount of additive added is generally between 1 and 3% by weight with respect to the weight 35 of the mix (aggregate/slag/additive/water); in this way, approximately 0.5 to 2.0% by weight of slag fines having a particle size of less than 80 μm are introduced into the mix.

The vitrified blast-furnace slag, which is added to the aggregates in the unpreground particulate state, may, according to the invention, be an as-granulated slag, which generally contains at most 5 approximately 1% fines, or an as-pelletized slag, which contains substantially no fines. Using an unpreground slag avoids having to grind all of the slag, something which constitutes a first advantage over the prior art. Furthermore, it is completely unnecessary to dry all of 10 the slag in order to avoid the reduction in the amounts of fines since the necessary fines are provided by the additive, so that the only fraction of slag to be dried is the ground slag which forms a constituent of the additive. However, it is possible to use a preground 15 slag instead of the as-produced particulate slag, accepting that the abovementioned first advantage would be lost, and, in this case, it is of little matter whether the fines of the preground slag remain during storage or not, since a sufficient and controlled 20 amount of slag fines is provided by the additive.

The subject of the present invention is also the additive for the construction of infrastructures according to the above process, characterized in that it includes, on the one hand, a pulverulent activator 25 and, on the other hand, dry ground vitrified slag having a particle size of less than 500 μm .

Preferably, the dry ground slag has a water content of less than 0.5% by weight.

Advantageously, the activator consists, for 30 more than 95% by weight, of lime, calcium sulphate or a mixture of lime and calcium sulphate; it may furthermore contain sodium or potassium hydroxide.

Preferably, the activator has an average particle size of between 0 and 500 μm and a moisture 35 content of less than 0.5% by weight.

Preferably, more than 95% by weight of the additive consists of a mixture having the following formulation by weight:

- calcium sulphate	25 to 45 %
- lime	2 to 6 %
- dry ground vitrified slag	qsp 100 %.

5 The additive may also contain known formulation
adjuvants for slag-based mixes in order to produce
infrastructures.

The illustrative and non-limiting example given
below will allow the invention to be more clearly
understood.

10 EXAMPLE:

The additive used has the following formulation
by weight:

- 36% calcium sulphate;
- 4% lime;
- 15 - 60% ground vitrified slag having a particle
size of less than 100 μm with a water content
of 0.5% by weight.

In order to construct a road infrastructure, a
mix having the following formulation is produced:

- 20 - 45% Seine (Anneville) fine siliceous-
limestone gravel (5 mm/20 mm) (IC 60);
- 45.5% of a Beauce (Baignolet) limestone sand
(less than 6 mm) (IC 100);
- 25 - 8% of an as-granulated slag produced from
haematite as iron ore (from Dunkerque) having
an activity coefficient of 23 according to
the NF P 98-108 standard;
- 1.5% of the additive defined above.

30 The various constituents of the mix are mixed
with water so as to obtain a mix having 8.7% water and
the mix is spread. Next, it is compacted until an PMO
density of 2.08 is obtained (PMO = "procto-modified
optimum").

35 The mechanical performance characteristics of
the compacted mix are measured as indicated below:

a) Post-setting strength:

Tensile strength tests were carried out on
vibro-compression test pieces having the dimensions
16 x 32 cm with the "Procto-modified optimum" (PMO)

parameters according to the NF P 98-114 standard at 90 days and at 360 days. The results are as follows:

90-day tensile strength (R _t)	0.73 MPa
360-day R _t	0.81 MPa
5 90-day elastic modulus E	14,880 MPa
360-day E	16,980 MPa

According to the NF P 98-118 standard, the mix is therefore classified as G2.

b) Workability time:

10 The test consists in measuring the speed of propagation of a wave through the material treated. The more it has hardened, the slower the speed.

15 The workability time is the time that elapses between an instant T₀ just after mixing, when the speed of propagation of the wave is v₀, and the instant when the speed is no more than 60% of v₀.

At a temperature of 20°C, a workability time of 15 hours 30 minutes was obtained.